

## HEAT TRANSFER IN OSCILLATING FLOW THROUGH POROUS MEDIUM WITH DISSIPATIVE HEAT

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In this paper, heat transfer in flow between two horizontal parallel porous plates through a porous medium when the upper plate oscillates in its own plane has been analyzed taking into account the effect of viscous dissipation. An increment in the Prandtl number or Reynolds number results in an increment of the temperature profile. With an increase in viscous dissipative heat the temperature distribution decreases.

**Key words:** injection, suction, transverse sinusoidal, transpiration cooling, viscous dissipation.

### 1. Introduction

The problem of Couette flow is applied in transpiration cooling. This technology is used in turbojet and rocket engines, exhaust nozzles and gas turbine blades. Gersten and Gross [1] studied a three dimensional flow and heat transfer past a porous plate by applying periodic suction. Singh [2] and Singh [3] studied a three dimensional flow and heat transfer along a porous plate. Singh *et al.* [4] studied a three dimensional free convection flow and heat transfer along a porous vertical plate. Guria and Jana [5] studied the unsteady three dimensional flow past a vertical porous plate subjected to time dependent periodic suction. The problem of transpiration cooling with the application of transverse sinusoidal injection/suction velocity distribution was studied by Singh [6]. Sing and Sharma [7] also studied a three dimensional Couette flow in the presence of a magnetic field. Guria and Jana [8] studied a unsteady three dimensional flow and heat transfer between two horizontal plates subjected to periodic suction. Guria *et al.* [9] extended this problem by applying oscillation of the upper plate in its own plane.

Flows through porous media have many application in chemical engineering for filtration and purification processes. A viscous flow past a porous plate through a porous medium was studied by Varshney [10]. An unsteady flow past a vertical porous plate through a porous medium was studied by Raptis [11]. Raptis and Perdakis [12] studied an oscillatory flow past a vertical porous plate through a porous medium. Singh and Sharma [13] investigated a three dimensional Couette flow and heat transfer through porous media. Singh and Sharma [14] investigated a three dimensional free convection flow and heat transfer past a vertical porous plate by applying periodic permeability. Guria *et al.* [15] studied a free convection flow through a porous medium bounded by vertical porous plates. Guria *et al.* [16] also studied a three dimensional Couette flow through porous media with an upper plate in its plane. Guria *et al.* [17] studied the effect of radiation on a three dimensional flow past a vertical porous plate through a porous medium. Guria [18] also studied the radiation effect on a three dimensional flow through a vertical channel embedded in a porous medium.

The objective of this paper is to study the heat transfer taking the viscous dissipative effect into account on flow between two infinite horizontal parallel porous plates through a porous medium, when the upper plates oscillates in its own plane. The velocity distribution has already obtained by Guria *et al.* [16].

## 2. Basic equations

Consider an unsteady flow between two infinite parallel flat porous plates through a porous medium separated at a distance  $d$ . The upper plate oscillates in its own plane with

$$u^* = U \left[ 1 + \epsilon e^{i\omega^* t^*} \right] \quad (2.1)$$

where  $\omega^*$  is the frequency of the oscillations,  $t^*$  is the time and  $U$  is the free stream velocity. The  $x^*$  axis is taken in the direction of the flow. The upper plate is subjected to a constant suction  $V_0$  and the lower plate to a transverse sinusoidal injection

$$v^* = -V_0 \left[ 1 + \epsilon \cos \left( \frac{\pi z^*}{d} \right) \right]. \quad (2.2)$$

Denoting velocity components  $u^*, v^*, w^*$  in the directions of the  $x^*, y^*$ , and  $z^*$  axes respectively, the flow is governed by the following equations

$$\frac{\partial v^*}{\partial y^*} + \frac{\partial w^*}{\partial z^*} = 0, \quad (2.3)$$

$$\frac{\partial u^*}{\partial t^*} + v^* \frac{\partial u^*}{\partial y^*} + w^* \frac{\partial u^*}{\partial z^*} = \nu \left( \frac{\partial^2 u^*}{\partial y^{*2}} + \frac{\partial^2 u^*}{\partial z^{*2}} \right) - \frac{\nu u^*}{K^*}, \quad (2.4)$$

$$\frac{\partial v^*}{\partial t^*} + v^* \frac{\partial v^*}{\partial y^*} + w^* \frac{\partial v^*}{\partial z^*} = -\frac{1}{\rho} \frac{\partial p^*}{\partial y^*} + \nu \left( \frac{\partial^2 v^*}{\partial y^{*2}} + \frac{\partial^2 v^*}{\partial z^{*2}} \right) - \frac{\nu v^*}{K^*}, \quad (2.5)$$

$$\frac{\partial w^*}{\partial t^*} + v^* \frac{\partial w^*}{\partial y^*} + w^* \frac{\partial w^*}{\partial z^*} = -\frac{1}{\rho} \frac{\partial p^*}{\partial z^*} + \nu \left( \frac{\partial^2 w^*}{\partial y^{*2}} + \frac{\partial^2 w^*}{\partial z^{*2}} \right) - \frac{\nu w^*}{K^*} \quad (2.6)$$

where  $\nu$  is the kinematic coefficient of viscosity,  $\rho$  is the density,  $p^*$  is the fluid pressure,  $K^*$  is the permeability of the porous medium.

The boundary conditions of the problem are

$$u^* = 0, \quad v^* = -V_0 \left[ 1 + \epsilon \cos \left( \frac{\pi}{d} z^* \right) \right], \quad w^* = 0 \quad \text{at} \quad y^* = 0, \quad (2.7)$$

$$u^* = U \left[ 1 + \epsilon e^{i\omega^* t^*} \right], \quad v^* = -V_0, \quad w^* = 0 \quad \text{at} \quad y^* = d.$$

Introducing the non-dimensional variables

$$y = \frac{y^*}{d}, \quad z = \frac{z^*}{d}, \quad t = ct^*, \quad p = \frac{p^*}{\rho U^2}, \quad u = \frac{u^*}{U}, \quad v = \frac{v^*}{U}, \quad w = \frac{w^*}{U}. \quad (2.8)$$

Eqs (2.3)-(2.6) become

$$\frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \quad (2.9)$$

$$\omega \frac{\partial u}{\partial t} + Re \left( v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = \left( \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) - \frac{u}{K}, \quad (2.10)$$

$$\omega \frac{\partial v}{\partial t} + Re \left( v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) = -Re \frac{\partial p}{\partial y} + \left( \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right) - \frac{v}{K}, \quad (2.11)$$

$$\omega \frac{\partial w}{\partial t} + Re \left( v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \right) = -Re \frac{\partial p}{\partial z} + \left( \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right) - \frac{w}{K} \quad (2.12)$$

where  $Re = Ud/v$  is the Reynolds number,  $S = V_0/U$  is the suction parameter and  $\omega = \omega^* d^2/v$  is the frequency parameter,  $K = K^*/d^2$  is the permeability parameter. Using Eqs (2.8), the boundary conditions (2.7) become

$$u = 0, \quad v = -S[1 + \epsilon \cos(\pi z)], \quad w = 0 \quad \text{at } y = 0, \quad (2.13)$$

$$u = (1 + \epsilon e^{i\omega t}), \quad v = -S, \quad w = 0 \quad \text{at } y = l.$$

### 3. Solution

We assume the solution of the given form

$$f(y, z, t) = f_0(y) + \epsilon f_1(y, z, t) + \epsilon^2 f_2(y, z, t) + \dots, \quad (3.1)$$

when  $\epsilon = 0$ , the solution is

$$v_0(y) = -S, \quad u_0(y) = \frac{(e^{-n_1 y} - e^{-n_2 y})}{(e^{-n_1} - e^{-n_2})} \quad (3.2)$$

where

$$n_{1,2} = \frac{l}{2} \left[ SRe \pm \{S^2 Re^2 + 4/K\}^{1/2} \right]. \quad (3.3)$$

When  $\epsilon \neq 0$ , the solution is

$$\begin{aligned}
u_l(y, z, t) = & \left[ C_9 e^{-r_1 y} + C_{10} e^{-r_2 y} + C_{11} e^{-(r_1+n_1)y} + C_{12} e^{-(r_2+n_1)y} + C_3 e^{(\pi-n_1)y} + \right. \\
& + C_4 e^{-(\pi+n_1)y} + C_5 e^{-(r_1+n_2)y} + C_6 e^{-(r_2+n_2)y} + C_7 e^{(\pi-n_2)y} + \\
& \left. + C_8 e^{-(\pi+n_2)y} \right] \cos \pi z + \frac{(e^{-m_1 y} - e^{-m_2 y})}{(e^{-m_1} - e^{-m_2})} e^{i\omega t},
\end{aligned} \tag{3.4}$$

$$v_l(y, z) = \left[ A e^{-r_1 y} + B e^{-r_2 y} + C e^{\pi y} + D e^{-\pi y} \right] \cos(\pi z), \tag{3.5}$$

$$w_l(y, z) = \frac{I}{\pi} \left[ A r_1 e^{-r_1 y} + B r_2 e^{-r_2 y} - C \pi e^{\pi y} + D \pi e^{-\pi y} \right] \sin(\pi z), \tag{3.6}$$

$$p_l(y, z) = S \left[ \left\{ C e^{\pi y} + D e^{-\pi y} \right\} - \frac{I}{K \pi Re} \left\{ C e^{\pi y} - D e^{-\pi y} \right\} \right] \cos(\pi z). \tag{3.7}$$

We omit the other constants. When  $K \rightarrow \infty$  the solutions coincide with the solution of Guria *et al.* [9]. The solution also exists for the blowing at the plate.

#### 4. Heat transfer

We consider the energy equation

$$\frac{\partial T^*}{\partial t^*} + v^* \frac{\partial T^*}{\partial y^*} + w^* \frac{\partial T^*}{\partial z^*} = \alpha \left( \frac{\partial^2 T^*}{\partial y^{*2}} + \frac{\partial^2 T^*}{\partial z^{*2}} \right) - \frac{\mu}{\rho C_p} \Phi^* \tag{4.1}$$

where  $\Phi^*$  is the viscous dissipation function given by

$$\Phi^* = 2 \left[ \left( \frac{\partial v^*}{\partial y^*} \right)^2 + \left( \frac{\partial w^*}{\partial z^*} \right)^2 \right] + \left( \frac{\partial u^*}{\partial y^*} \right)^2 + \left( \frac{\partial w^*}{\partial y^*} + v^* \frac{\partial v^*}{\partial z^*} \right)^2 + \left( \frac{\partial u^*}{\partial z^*} \right)^2 \tag{4.2}$$

where  $C_p$  is the specific heat at constant pressure,  $\mu$  is the viscosity,  $\alpha$  is the thermal conductivity of the fluid.

The temperature boundary condions are

$$T^* = T_0 \quad \text{at } y^* = 0 \quad \text{and} \quad T^* = T_l \quad \text{at } y^* = d. \tag{4.3}$$

Introducing

$$\theta = \frac{T^* - T_0}{T_l - T_0}, \tag{4.4}$$

Eq.(4.1) becomes

$$Pr\omega \frac{\partial \theta}{\partial t} + RePr \left( v \frac{\partial \theta}{\partial y} + w \frac{\partial \theta}{\partial z} \right) = \left( \frac{\partial^2 \theta}{\partial y^2} + \frac{\partial \theta}{\partial z^2} \right) + PrEc\Phi \quad (4.5)$$

where

$$\Phi = 2 \left[ \left( \frac{\partial v}{\partial y} \right)^2 + \left( \frac{\partial w}{\partial z} \right)^2 \right] + \left( \frac{\partial u}{\partial y} \right)^2 + \left( \frac{\partial w}{\partial y} + v \frac{\partial v}{\partial z} \right)^2 + \left( \frac{\partial u}{\partial z} \right)^2. \quad (4.6)$$

The temperature boundary conditions become

$$\theta(0) = 0, \theta(1) = 1. \quad (4.7)$$

We assume the solution of the temperature equation in the form

$$\theta(y, z, t) = \theta_0(y) + \epsilon \theta_1(y, z, t) + \epsilon^2 \theta_2(y, z, t) + \dots \quad (4.8)$$

Substituting  $\theta$  in (4.5) and comparing the term free of  $\epsilon$ , we get

$$\theta_0'' + SRePr\theta_0' = -PrEcu_0'^2 \quad (4.9)$$

where

$$\theta_0(0) = 0 \quad \text{and} \quad \theta_0(1) = 1. \quad (4.10)$$

The zeroth order solution is given by

$$\theta_0(y) = d_1 e^{-2n_1 y} + d_2 e^{-2n_2 y} + d_3 e^{-SRey} + d_4 + d_5 e^{-SRePr y}, \quad (4.11)$$

where

$$\begin{aligned} K_2 &= \frac{-PrEc}{(e^{n_1} - e^{-n_2})^2}, \quad d_1 = \frac{K_2 n_1^2}{2n_1(2n_1 - SRePr)}, \quad d_2 = \frac{K_2 n_2^2}{2n_2(2n_2 - SRePr)}, \\ d_2 &= \frac{K_2 n_2^2}{2n_2(2n_2 - SRePr)}, \quad d_3 = \frac{2K_2}{KS^2 Re^2 (1 - Pr)}, \\ d_4 &= \frac{1}{(1 - e^{-SRePr})} \left[ 1 - d_1 (e^{-2n_1} - e^{-SRePr}) + \right. \\ &\quad \left. - d_2 (e^{-2n_2} - e^{-SRePr}) - d_3 (e^{-SRe} - e^{-SRePr}) \right], \\ d_5 &= \frac{-1}{(1 - e^{-SRePr})} \left[ 1 - d_1 (e^{-2n_1} - 1) - d_2 (e^{-2n_2} - 1) - d_3 (e^{-SRe} - 1) \right]. \end{aligned} \quad (4.12)$$

Comparing the coefficient of  $\epsilon$ , we get

$$Pr \frac{\partial \theta_I}{\partial t} + RePr \left( v_I \frac{\partial \theta_0}{\partial y} + v_0 \frac{\partial \theta_I}{\partial z} \right) = \left( \frac{\partial^2 \theta}{\partial y^2} + \frac{\partial \theta}{\partial z^2} \right) + 2PrEcu_0' u_1'. \quad (4.13)$$

Assuming

$$\theta_I(y, z, t) = \theta_{11}(y) \cos \pi z + \theta_{12}(y) e^{i\omega t} \quad (4.14)$$

and substituting Eq.(4.14) in Eq.(4.13), we get

$$\theta_{11}'' + SRePr\theta_{11}' - \pi^2 \theta_{11} = RePr\theta_0' v_{11} - 2PrEcu_0' u_{11}', \quad (4.15)$$

$$\theta_{12}'' + SRePr\theta_{12}' - i\omega Pr\theta_{12} = -2PrEcu_0' u_{12}', \quad (4.16)$$

where

$$\theta_{11}(0) = 0, \quad \theta_{12}(0) = 0 \quad \text{and} \quad \theta_{11}(1) = 0, \quad \theta_{12}(1) = 0. \quad (4.17)$$

The first order solution is given by

$$\begin{aligned} \theta_I(y, z, t) = & \left[ L e^{-m_5 y} + M e^{-m_6 y} + A_1 e^{-(r_1 + SRePr)y} + A_2 e^{-(r_2 + SRePr)y} + \right. \\ & + A_3 e^{(\pi - SRePr)y} + A_4 e^{-(\pi + SRePr)y} + A_5 e^{-(r_1 + 2n_1)y} + A_6 e^{-(r_2 + 2n_1)y} + \\ & + A_7 e^{(\pi - 2n_1)y} + A_8 e^{-(\pi + 2n_1)y} + A_9 e^{-(r_1 + 2n_2)y} + A_{10} e^{-(r_2 + 2n_2)y} + \\ & + A_{11} e^{(\pi - 2n_2)y} + A_{12} e^{-(\pi + 2n_2)y} + A_{13} e^{-(r_1 + SRe)y} + A_{14} e^{-(r_2 + SRe)y} + \\ & + A_{15} e^{(\pi - SRe)y} + A_{16} e^{-(\pi + SRe)y} + A_{17} e^{-(r_1 + n_1)y} + A_{18} e^{-(r_1 + n_2)y} + \\ & \left. + A_{19} e^{-(r_2 + n_1)y} + A_{20} e^{-(r_2 + n_2)y} \right] \cos(\pi z) + \left[ L_1 e^{-m_3 y} + M_1 e^{-m_4 y} + \right. \\ & \left. + B_1 e^{-(m_1 + n_1)y} + B_2 e^{-(m_2 + n_2)y} + B_3 e^{-(m_2 + n_1)y} + B_4 e^{-(m_1 + n_2)y} \right] e^{i\omega t}, \end{aligned} \quad (4.18)$$

where

$$m_{3,4} = \frac{SRePr \pm \sqrt{S^2 Re^2 Pr^2 + 4i\omega Pr}}{2}, \quad m_{5,6} = \frac{SRePr \pm \sqrt{S^2 Re^2 Pr^2 + 4\pi^2}}{2}. \quad (4.19)$$

The other constants are not given here to save space.

## 5. Results and discussion

Variations of  $\theta$  for several values of the Eckert number  $Ec$ , Prandtl number  $Pr$  and Reynolds number  $Re$  are shown in Figs 1-3. It is found that with an increase in either  $Re$ ,  $Pr$  the temperature profile  $\theta$  increases. With an increase in the viscous dissipative heat the temperature distribution decreases. It is observed that with an increase in the Prandtl number the temperature of the flow increases at all points.

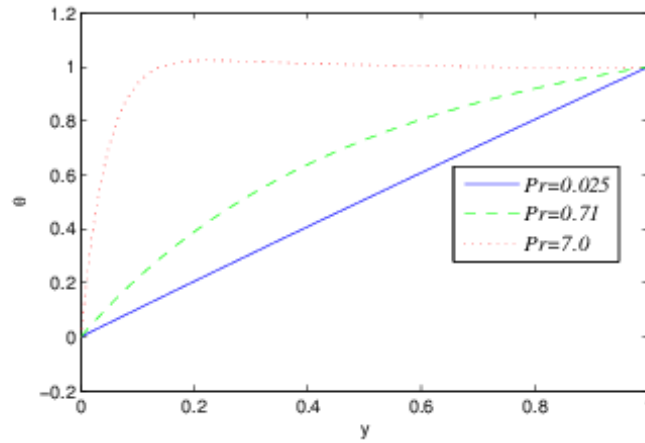


Fig.1. Variation of  $\theta$  for  $\omega t = 45^\circ$ ,  $S = 0.5$ ,  $K = 2$ ,  $\omega = 5$ ,  $Ec = 0.1$ ,  $\epsilon = 0.25$ .

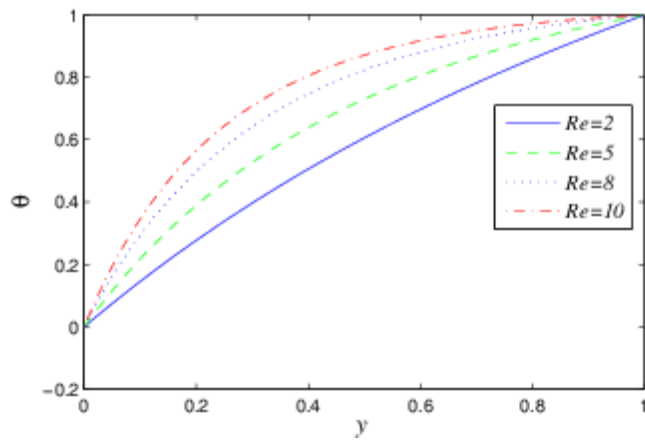


Fig.2. Variation of  $\theta$  for  $\omega t = 45^\circ$ ,  $S = 0.5$ ,  $K = 2$ ,  $Ec = 0.1$ ,  $Pr = 0.71$ ,  $\epsilon = 0.25$ .

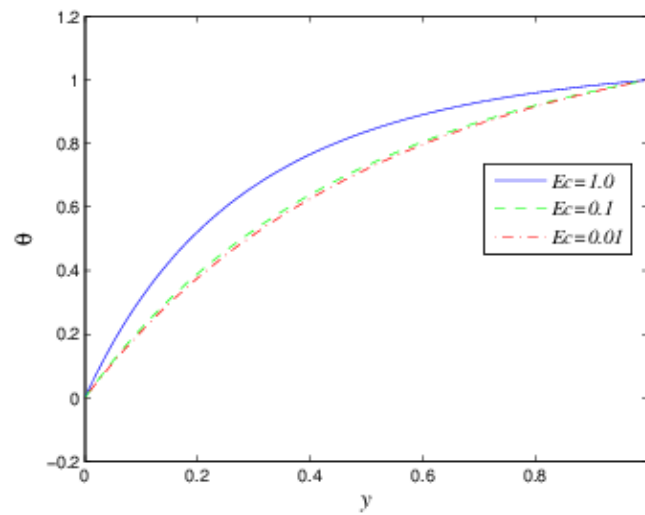


Fig.3. Variation of  $\theta$  for  $\omega t = 45^\circ$ ,  $S = 0.5$ ,  $K = 2$ ,  $\omega = 5$ ,  $Re = 5$ ,  $\epsilon = 0.25$

The rate of heat transfer from the plate to the fluid may be calculated using the formula

$$q = -k \left( \frac{\partial T^*}{\partial y^*} \right)_{y^*=0} = -\frac{k(T_w - T_0)}{d} \left( \frac{\partial \theta}{\partial y} \right)_{y=0}. \quad (5.1)$$

In a non-dimensional form the heat transfer coefficient at the plate  $y = 0$  is given by

$$\begin{aligned} Nu &= \frac{qd}{k(T_w - T_0)} = -\left( \frac{\partial \theta}{\partial y} \right)_{y=0} = -\theta'_0(0) - \epsilon \theta'_1(0), \\ Nu &= -\theta'_0(0) - \epsilon \left[ \theta'_{11}(0) \cos \pi z + \theta'_{12}(0) e^{i\omega t} \right], \\ Nu &= -\theta'_0(0) - \epsilon \left[ \theta'_{11}(0) \cos \pi z + H_1 \cos(\phi_1 + \omega t) \right]. \end{aligned} \quad (5.2)$$

Variations of amplitude and tangent of phase shift in terms of the Nusselt number for several values of frequency parameter  $\omega$  and Reynolds number  $Re$  is shown in Tab.1. It is seen that the amplitude and tangent of phase shift decreases with increase in either  $Re$  or  $\omega$ . It is observed that due to high frequency of oscillations of the plate, the magnitude of the rate of heat transfer reduces. The values of  $\tan \phi_1$  show that there is a phase lead for lower frequency in the rate of heat transfer coefficient.

Table 1. The amplitude  $H_1$  and phase shift  $\tan \phi_1$  of the Nusselt number  $S = 0.5$ ,  $Pr = 0.71$ ,  $\epsilon = 0.25$ ,  $\omega t = 45^\circ$ .

$Re$	$H_1$			$\tan \phi_1$		
	$\omega = 2$	$\omega = 5$	$\omega = 10$	$\omega = 2$	$\omega = 5$	$\omega = 10$
1	1.76	1.28	0.59	33.01	36.21	11.08
1.5	1.46	1.42	0.64	12.58	17.62	8.19
2	0.94	1.34	0.62	5.87	9.94	5.63
2.5	0.41	1.04	0.49	2.11	5.63	3.36

## 6. Conclusion

The temperature distribution in a flow between two horizontal parallel porous plates through a porous medium has been obtained in the presence of viscous dissipative heat. It is found that with an increase in either Reynolds or Prandtl number the temperature profile increases but it decreases with an increase in the Eckert number. The rate of heat transfer has also been obtained in terms of the Nusselt number. It is seen that the amplitude and tangent of phase shift decreases with an increase in either the Reynolds number or frequency parameter. With an increase in the viscous dissipative heat the temperature distribution decreases. It is observed that increasing the Prandtl number increases temperature of the flow at all points. It is observed that due to a high frequency of oscillations of the plate, the magnitude of the rate of heat transfer reduces. The values of  $\tan \phi_1$  show that there is a phase lead for lower frequency in the rate of heat transfer coefficient.

## Nomenclature

$A_i$   $i = 1, \dots, 20$  – constants



- $A, B, C, D$  – constants  
 $C_i, i = 1, \dots, 10$  – constants  
 $C_p$  – specific heat at constant pressure  
 $d_i, i = 1, \dots, 5$  – constants  
 $d$  – channel width  
 $Ec$  – Eckert number  
 $g$  – gravitational acceleration  
 $Gr$  – Grashof number  
 $K$  – permeability parameter  
 $K_1, K_2$  – constant  
 $m_i, i = 1, \dots, 6$  – constants  
 $Nu$  – Nusselt number at the left plate  
 $p^*$  – pressure  
 $p$  – dimensionless pressure  
 $Pr$  – Prandtl number  
 $q$  – local heat transfer at the plate  
 $r_i, i = 1, \dots, 4$  – constants  
 $Re$  – Reynolds number  
 $T^*$  – temperature of the fluid  
 $T_w$  – plate temperature ( $y^* = 0$ )  
 $T_0$  – plate temperature ( $y^* = d$ )  
 $u^*, v^*, w^*$  – velocity components in  $x, y, z$  axes  
 $u, v, w$  – dimensionless Velocity components in  $x, y, z$  axes respectively  
 $V_0$  – constant suction velocity  
 $x^*, y^*, z^*$  – Cartesian coordinates system;  
 $x, y, z$  – dimensionless Cartesian coordinate system  
 $\mu$  – viscosity  
 $\beta$  – coefficient of thermal expansion  
 $\theta$  – non-dimensional temperature  
 $\nu$  – kinematic viscosity  
 $\varepsilon$  – amplitude of the suction velocity  
 $\rho$  – density of the fluid

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